

(19)



Europäisches Patentamt
European Patent Office
Office européen des brevets



(11) Publication number:

0 650 216 A1

(12)

EUROPEAN PATENT APPLICATION(21) Application number: **94116815.5**(51) Int. Cl.⁶: **H01Q 7/08, H01Q 23/00**(22) Date of filing: **25.10.94**(30) Priority: **26.10.93 US 143263**(43) Date of publication of application:
26.04.95 Bulletin 95/17(84) Designated Contracting States:
DE FR GB IT NL(71) Applicant: **TEXAS INSTRUMENTS
DEUTSCHLAND GMBH
Haggertystrasse 1
D-85350 Freising (DE)**(72) Inventor: **Knebelkamp, Michael c/o Texas Inst.
Deutschl. GmbH
Haggertystrasse 1, M/S 4297
D-85350 Freising (DE)**(74) Representative: **Schwepfinger, Karl-Heinz,
Dipl.-Ing. et al
Prinz & Partner,
Manzingerweg 7
D-81241 München (DE)**(54) **Antenna circuit.**

(57) An alternative resonant circuit configuration which reduces the amount of RF current that is switched by the power-stage transistors of a T/R unit and thereby also significantly reduces the reliability risk is disclosed. A parallel resonant antenna configuration of coils and capacitors reduces the RF current through the output stage push-pull transistor configuration to a small fraction of the RF current experienced by typical series resonant circuits. This circuit offers advantages of low cost, reliable impedance matching while reducing the volume necessary to perform the function.

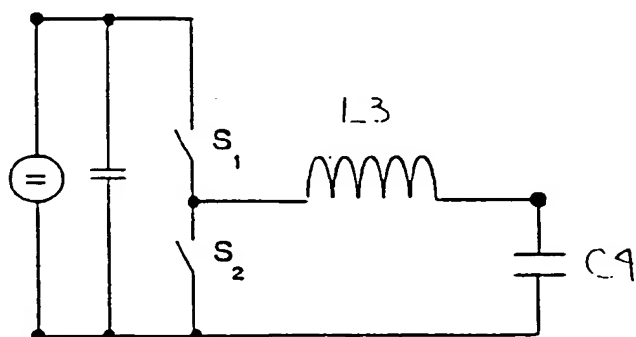


FIG. 1

BEST AVAILABLE COPY

FIELD OF THE INVENTION

This invention generally relates to antenna circuits, suitable for high and low power applications, which do not require use of transformers.

BACKGROUND OF THE INVENTION

To remotely charge up a transponder in a RF identification system, the transmit/receive (T/R) unit must transmit a high magnetic field strength. A magnetic field instead of an electric field is used because the energy density is much higher than in an electrical field. The principle at work can be compared to a simple transformer with the T/R unit coil being the primary part and the transponder coil being the secondary part. The magnetic field couples to the transponder from the T/R unit with a large air gap in between. In view of the above description, a magnetic field may be generated with a series combination of a simple coil and generator. However, with this configuration, a high field strength is only generated if many windings are used, because the magnetic field is proportional to the number of windings.

Therefore, in order to generate high currents, resonance is used and a series capacitor can be added to the generator/coil configuration of the T/R unit. In an ideal series resonance circuit, with a high quality factor, the voltage drop at the antenna (coil) and thus the current through the antenna is multiplied by the quality factor, Q. A Q of 100, for example, generates a voltage at the antenna that is 100 times the value applied to the resonance circuit and the current is multiplied by the same value. In this way, high currents yielding high magnetic field strengths are generated.

This magnetic field is oftentimes generated by either a series or parallel resonant circuit in the T/R unit. When an AC voltage with the resonant frequency is applied to the tuned antenna circuit, the resonant circuit behaves as a very low ohmic resistance, i.e. the D.C. resistance of the antenna coil, allowing the coil of the resonant circuit to efficiently transmit the energy applied. At resonance, an ideal series resonant circuit will appear to the output stage to be a short circuit (impedance = 0 ohms) which could cause damage to the output stage. Therefore, the driver circuit must have the capability to drive this low impedance. A transformer can be used to adapt the power-stage of the T/R unit to the low impedance of the resonance circuit, to protect the driver circuit and determine the amount of power that is transferred to the resonator circuit via the ratio of windings. If a transformer is not used, the minimum allowed D.C. resistance of the antenna coil must be specified to ensure that the low impedance of the load does not destroy the driver. However, there are also several disadvantages to using a transformer, including high cost and high-volume requirements both of which are undesirable in ever increasingly smaller-size production modules.

A possible configuration of a circuit which eliminates the transformer is shown in Figure 1. There are many different ways to realize the generation of an AC voltage in the T/R unit and one of the more common methods is through use of a push-pull stage. A push-pull stage can be realized with traditional field effect transistors. These transistors are characterized by a low 'on' resistance and thus exhibit low power loss and an ability to handle large currents. In addition, transistors are very cost effective components. The circuit shown in Figure 1 consists of a push-pull stage, consisting of a series connected transistor pair depicted as switches S1 and S2, and a series resonant circuit, consisting of an inductor L3 and a capacitor C4.

A significant disadvantage of this circuit is that the transistors S1 and S2, have to switch the complete RF current that is generated when an AC voltage with the resonant frequency is applied to the tuned antenna circuit. In high power applications, i.e. 400 volts peak to peak voltage, the large amounts of RF current generated make the transistors very, very hot and increase the chance for transistor breakdown (exceed the maximum specified current value). This may decrease the reliability of the T/R unit and may reduce the effectiveness of the reader transmission. Moreover, a large heat-sink is oftentimes required to reduce the heating, and heat sinks require great amounts of volume. The heating of the transistors may also reduce the maximum ambient temperature of the entire reader as the maximum temperature of other reader components may be limited.

SUMMARY OF THE INVENTION

An alternative circuit configuration which reduces the amount of RF current that is switched by the power-stage transistors and thereby also significantly reduces the reliability risk is shown in Figure 2. Instead of the simple series resonant circuit of Figure 1 connected to the transistors of the power stage, the slightly more complex configuration of coils and capacitors of Figure 2 reduces the RF current through, for example, S2, to a small fraction of the RF current experienced by the same switch S2 in Figure 1.

BEST AVAILABLE COPY

Many advantages are offered by this circuit configuration versus other known circuit configurations in the art. The first advantage offered is the alleviation of the transformer requirement. Transformers are expensive and large in size and therefore not very feasible for small production type modules. Therefore, removing the need for a transformer gains a significant cost saving as well as reduces the amount of space needed to match the power-stage of the transmitter to the antenna circuit.

A second advantage offered is the reduction in the switching current flowing through the output push-pull stage transistors. With the circuit shown in Figure 2, transistors of the output push-pull stage have to switch only a fraction of the RF current that the output push-pull stage of Figure 1 would have to switch.

A yet third advantage is the flexibility the circuit configuration in Figure 2 offers to choose the physical position of the larger, high-volume capacitors C1 and C2. Capacitors C1 and C2 could conceivably be a part of the RF module or a part of the antenna, due to the way in which they are connected to the rest of the circuit in Figure 2. The voltage drop at the capacitor C3 is nearly a sine wave (the push-pull generates a rectangular voltage) and relatively long cables can be used to connect the second part of the main antenna circuit without the risk of generating electromagnetic interference (for example, by harmonics of a rectangular voltage).

BRIEF DESCRIPTION OF THE DRAWINGS

The invention will be explained in greater detail with reference to an example of an embodiment shown in the drawings, in which:

Figure 1 shows a circuit schematic of an antenna matching circuit which alleviates the need for a transformer.

Figure 2 shows a circuit schematic, according to this invention, of a matching circuit which significantly reduces the amount of current the switching transistors must handle.

Figure 3 shows an equivalent circuit of Figure 1 assuming switch S2 is closed and switch S1 is open.

Figure 4 shows an equivalent circuit of Figure 2 assuming switch S1 is open and switch S2 is closed.

DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

The circuit on the left-hand side of Figure 2 is a schematic of the AC source in the T/R unit realized with a battery 10, a large capacitor 12 and the push-pull stage 14. The circuit on the right hand-side of Figure 2 is a preferred embodiment of the improved antenna circuit. This antenna circuit allows only a fraction of the RF current which switches through S1 in Figure 1, to switch through S1 in Figure 2.

The antenna circuit of Figure 2 can be divided into two parts. A high-impedance part comprised of capacitors C1, C2 and inductor L1, and a low impedance part comprised of inductor L2 and capacitor C3. The series resonant circuit of inductor L2 and capacitor C3 has a low defined Q that the push-pull stage 14 can drive. Moreover, the low Q series resonant circuit of inductor L2 and capacitor C3 also stimulates the main antenna circuit of L1, C2, and C1. The better the low Q series resonant circuit (L2,C3) is tuned to the resonant frequency of 134.2 KHz, the more the circuit behaves as a low ohmic resistor if connected to an AC voltage with the same resonant frequency. Therefore, the tuning of the low Q part of the antenna circuit (L2,C3) determines the amount of power applied to the main antenna circuit of L1, C2, and C1. Connecting C2, and C1 and L1 to the combination of L2 and C3 as shown in Figure 2, C1, C2, C3 and L1 constitute a parallel resonant circuit. This circuit can also be tuned to the desired resonant frequency by choosing the appropriate value of capacitors C1 and C2. The impedance of the complete circuit is given by the formula:

$$Z_{\epsilon} = j\Omega L_2 + \frac{(1 - \Omega^2 L_1(C_1 + C_2))}{(j\Omega C_3(1 - \Omega^2 L_1(C_1 + C_2)) + j\Omega C_2(1 - \Omega^2 L_1 C_1))}$$

where $W = 2\pi f$, and f = frequency.

As previously mentioned, the power stage of the transmitter can be a simple push-pull stage as indicated. One advantage of this antenna circuit is that the transistors of the push-pull stage only have to switch a fraction of the RF current. Switching only a fraction of the RF current greatly reduces heating up the transistors.

A comparison of the circuit configurations given in Figure 1 and Figure 2 is given in Figures 3 and 4. Figures 3 and 4 are equivalent circuit configurations of Figures 1 and 2, assuming that switch S2 is closed,

and switch **S1** is open. As can be seen in Figure 3, switch **S2** must switch the entire RF current, as there exists a single path for current to flow in Figure 3. However, as shown in Figure 4, switch **S2** must only switch 1/6th (for high power choice of components below) of the entire RF current, as there are several current paths in Figure 4.

The maximum amount of energy that is applied to the main resonant circuit which corresponds to the generated magnetic field strength, can be regulated by the value of **L2** or **C3**. For example, for a low power application, i.e. for a peak antenna voltage of approximately 200 volts, the following components are possible;

L1 = 27.7 mH, **L2** = 2.7 mH, **C1** = 23.5 nF, **C2** = 23.5 nF, and **C3** = 1.36 uF. For a high power application, i.e. for a peak antenna voltage of approximately 400 volts, **C3** should be changed to 880 nF.

A few preferred embodiments have been described in detail hereinabove. It is to be understood that the scope of the invention also comprehends embodiments different from those described, yet within the scope of the claims.

While this invention has been described with reference to illustrative embodiments, this description is not intended to be construed in a limiting sense. Various modifications and combinations of the illustrative embodiments, as well as other embodiments of the invention, will be apparent to persons skilled in the art upon reference to the description. It is therefore intended that the appended claims encompass any such modifications or embodiments.

Claims

1. An antenna resonant circuit of a transmit/receive unit which reduces the amount of current flowing through the output-power stage of the unit comprising:
a resonant circuit for stimulating a main antenna circuit to oscillate with a resonant frequency;
a main antenna circuit; and
wherein said resonant circuit is connected in parallel with said output power stage of said transmit/receive unit.
2. The antenna resonant circuit of claim 1, wherein the resonant circuit is a low quality factor series resonant circuit comprising a first capacitor and a first inductor connected in series.
3. The antenna resonant circuit of claim 2, wherein the amount of power transferred from the low Q series resonant circuit to the main antenna resonant circuit is determined by the values of the inductor and the capacitor of the resonant circuit.
4. The antenna resonant circuit of claim 2 or claim 3, wherein the main antenna circuit comprises a second capacitor and a second inductor in parallel and a series combination of said first capacitor and a third capacitor.
5. The antenna resonant circuit of claim 4, wherein said resonant frequency of said antenna resonant circuit is determined by the values of the second and third capacitor.
6. The antenna resonant circuit of any preceding claim, wherein said output power stage comprises a push-pull pair of transistors.
7. The antenna resonant circuit for use in an RF identification system.
8. An RF identification system including an antenna resonant circuit according to any of claims 1 to 6.
9. A transmit/receive unit comprising an antenna resonant circuit according to any of claims 1 to 6.

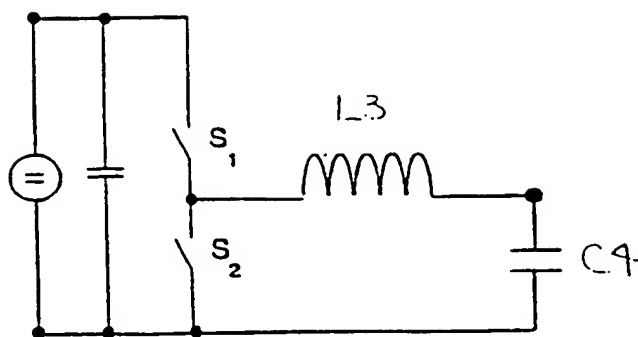


FIG. 1

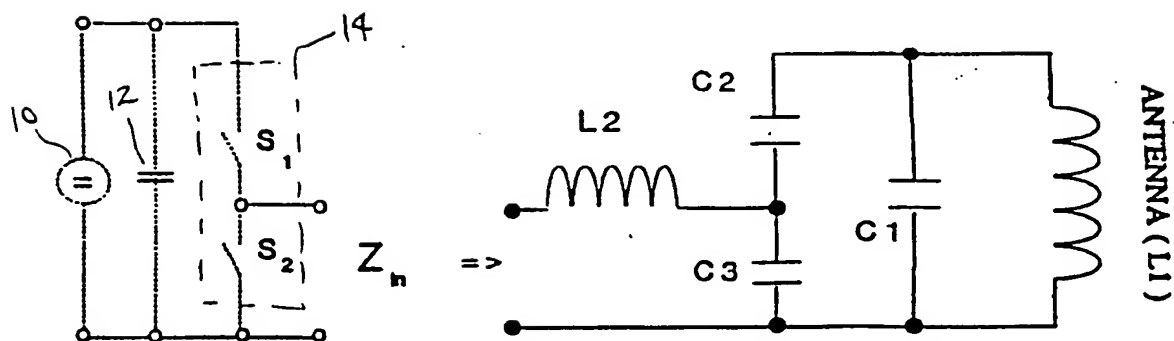


FIG. 2

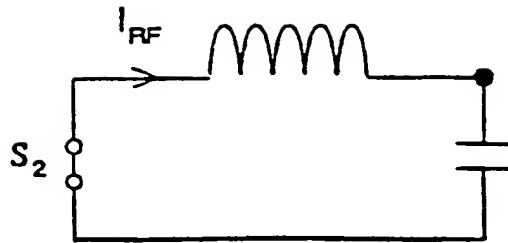


FIG. 3

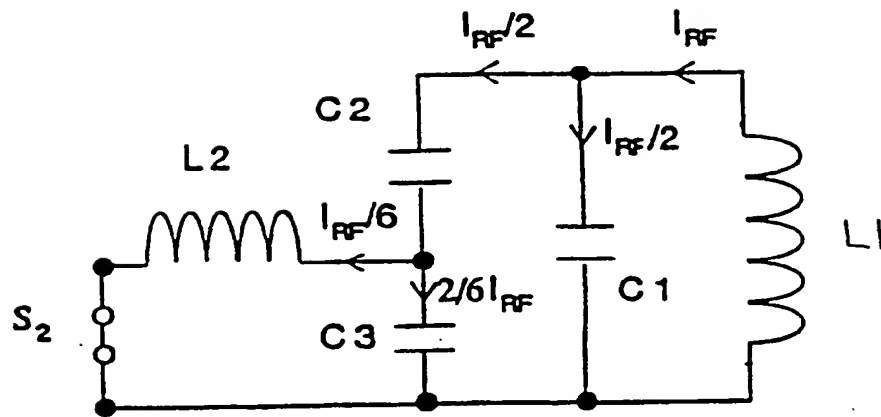


FIG. 4



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 94 11 6815

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
X	EP-A-0 365 939 (COMPAGNIE GENERALE DES ETABLISSEMENTS MICHELIN-MICHELIN & CIE) * the whole document * ---	1-9	H01Q7/08 H01Q23/00
A	EP-A-0 523 271 (TEXAS INSTRUMENTS DEUTSCHLAND GMBH) * the whole document * ---	1-9	
A	EP-A-0 523 272 (TEXAS INSTRUMENTS DEUTSCHLAND GMBH) * the whole document * -----	1-9	
			TECHNICAL FIELDS SEARCHED (Int.Cl.6)
			H01Q H03H
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 10 February 1995	Examiner Deconinck, E
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application I : document cited for other reasons & : member of the same patent family, corresponding document			

EPO FORM 1503 03.92 (PM/C01)